# UNCLASSIFIED

AD 296 850

Reproduced by the

ARMED SERVICES TECHNICAL INFORMATION AGENCY
ARLINGTON HALL STATION
ARLINGTON 12, VIRGINIA



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

# 296 850

296850

# OFFICE OF NAVAL RESEARCH

Contract Nonr 562(25)

NR-064-431

Technical Report No. 18

ARIATIONAL PRINCIPLES IN THE LINEAR THEORY OF VISCOELASTICITY

by

M. E. Gurtin

DIVISION OF APPLIED MATHEMATICS

**BROWN UNIVERSITY** 

PROVIDENCE, R. I.

January 1963

Variational principles in the linear theory of viscoelasticity\*

bу

#### M. E. Gurtin

#### Brown University

#### 1. <u>Introduction</u>

The object of this paper is to supply generalizations to linear quasi-static viscoelasticity theory of certain variational principles which characterize the solution of the mixed boundary-value problem of classical elastostatics. This problem consists in finding a "state" - i.e. a displacement, strain, and stress field - which satisfies the governing field equations in a given region of space and meets the standard mixed boundary conditions. The relevant field equations consist of the displacement-strain relations, the stress-strain relations, and the stress equations of equilibrium; whereas the boundary conditions involve the prescription of displacements over a portion of the boundary and of surface tractions over the remainder.

Two of the most important variational principles applicable to the foregoing problem are the principle of stationary potential energy and the principle of stationary complementary energy. The former asserts that the variation of the "potential energy" over the set of all kinematically admissible states is

The results communicated in this paper were obtained in the course of an investigation conducted under Contract Nonr-562(25) of Brown University with the Office of Naval Research in Washington, D. C.

See, for example, Sokolnikoff [1](Articles 107, 108). If the elastic constants are such that the strain energy density is a positive definite function of the strains then these variational principles imply corresponding minimum principles.

By a kinematically admissible state we mean a state that satisfies the displacement-strain relations, the stress-strain relations, and the displacement boundary conditions.

zero at a certain state <u>if</u> and <u>only if</u> that state is a solution of the mixed problem under consideration.

On the other hand the principle of stationary complementary energy asserts that the variation of the "complementary energy" over the set of all statically admissible stress fields is zero at a certain stress field if that stress field belongs to the solution of the mixed problem. Southwell [2] and Langhaar [3] proved a converse of this theorem on the assumption that the tractions are prescribed over the entire boundary and the region is simply connected: the variation of the "complementary energy" over the set of all statically admissible stress fields is zero at a stress field only if that stress field belongs to the solution of the problem at hand. For the case in which displacements are prescribed over a portion of the boundary a similar converse follows from a slight modification of a theorem due to Dorn and Schild [4].

Various extensions of the preceding variational principles of elastostatics have been established in which the class of admissible states is subjected to weaker restrictions. One extension of this kind was given by Hellinger [5] and was later independently discovered in a somewhat stronger form by Reissner [6],[7].

<sup>3</sup> By a statically admissible stress field we mean a stress field that meets the stress equations of equilibrium as well as the traction boundary conditions.

<sup>4</sup> See Section 4 for a statement and proof of the modified theorem.

This principle asserts that the variation of a certain functional over the set of all states which meet the strain-displacement relations is zero at a particular state if and only if that state is a solution of the mixed problem. Apparently guided by Reissner's improved version of Hellinger's theorem, Hu Hai-chang [8] and Washizu [9] separately arrived at a still broader variational principle which does not require the admissible states to meet any of the field equations or boundary conditions.

This paper aims at variational principles for linear viscoelasticity which generalize the foregoing results of classical elastostatics. Although variational principles for viscoelasticity theory were considered previously by Biot [10], Freudenthal and Geiringer [11], and Onat [12], these investigations do not arrive at generalizations of the type sought here.

The present paper is a continuation of a recent study
[13] which contains a systematic treatment of linear viscoelasticity theory based on the notion of a Stieltjes convolution.

Section 2 contains certain preliminary definitions and notational agreements. In Section 3 variational principles appropriate to the linear quasi-static theory of viscoelastic solids are given for the case in which the stress-strain relations are in relaxation integral form. Section 4 is devoted to the derivation of analogous results for stress-strain relations in creep integral form. In the variational principles established here the viscoelastic solid is allowed to be inhomogeneous and anisotropic and the relevant stress, strain, and displacement histories are permitted to possess finite jump discontinuities in time.

#### 2. Notation. Preliminary definitions.

Throughout what follows R will denote an open region of three-dimensional Euclidean space with the closure  $\overline{R}$  and the boundary B. Further  $\underline{n}$  will denote the unit outward normal to B and  $B_{\alpha}$  ( $\alpha=1,2$ ) will denote complementary subsets<sup>5</sup> of B (B =  $B_1 \cup B_2$ ,  $B_1 \cap B_2 = 0$ ). Finally, the symbol "x" will be used to indicate the cartesian product of two sets.

Let  $u_1, \varepsilon_{ij}, \sigma_{ij}, F_i, G_{ijk\ell}$ , and  $J_{ijk\ell}$ , in this order, designate the cartesian components of the displacement vector  $\underline{u}$ , the strain tensor  $\underline{\varepsilon}$ , the stress tensor  $\underline{\sigma}$ , the body force (density) vector  $\underline{F}$ , the relaxation tensor  $\underline{G}$ , and the creep tensor  $\underline{J}$ . All of the preceding field histories, including  $\underline{G}$  and  $\underline{J}$ , are to be regarded as functions of position and time defined on  $R\times(-\infty,\infty)$ . With this notation the complete system of field equations in the linear quasi-static theory of (inhomogeneous and anisotropic) viscoelastic solids take the form

$$2\varepsilon_{i,j} = u_{i,j} + u_{j,i}$$
 on  $R\times(-\infty,\infty)$ , (2.1)

$$\sigma_{ij,j} + F_i = 0$$
,  $\sigma_{ij} = \sigma_{ji}$  on  $RX(-\infty, \infty)$ , (2.2)

and either

$$\sigma_{ij} = G_{ijk\ell} * d\varepsilon_{k\ell}$$
 on  $Rx(-\infty, \infty)$ , (2.3)

or

$$\varepsilon_{ij} = J_{ijk\ell} * do_{k\ell}$$
 on  $Rx(-\infty, \infty)$ . (2.4)

Henceforth the subscript  $\alpha$  will be understood to have the range of the integers (1,2).

We use the usual indicial notation. Thus Latin subscripts have the range of the integers (1,2,3) and summation over repeated subscripts is implied; subscripts preceded by a comma indicate differentiation with respect to the corresponding cartesian coordinate.

Equations (2.1) are the linearized <u>strain-displacement relations</u>, (2.2) are the <u>stress equations of equilibrium</u>, (2.3) represent the <u>stress-strain relations in relaxation integral form</u>, while (2.4) represent the <u>stress-strain relations in creep integral form</u>. In writing (2.3), (2.4) we have made use of the notation for Stieltjes convolutions introduced previously in [13]. Thus, if f and g are functions of position and time, f\*dg stands for the function defined by the Stieltjes integral

$$[f*dg](\underline{x},t) = \int_{\tau=-\infty}^{t} f(\underline{x},t-\tau)dg(\underline{x},\tau), \qquad (2.5)$$

provided this integral is meaningful. To the system of field equations just cited we adjoin the <u>initial</u> <u>conditions</u>

$$\underline{\mathbf{u}} = \underline{\boldsymbol{\varepsilon}} = \underline{\boldsymbol{\sigma}} = 0 \quad \text{on} \quad \mathbb{R} \times (-\infty, 0),$$
 (2.6)

the <u>displacement</u> boundary conditions

$$\underline{\mathbf{u}} = \underline{\hat{\mathbf{u}}} \quad \text{on} \quad \mathbf{B}_{1} \times (-\infty, \infty),$$
 (2.7)

and the traction boundary conditions

$$\underline{S} = \hat{\underline{S}} \quad \text{on} \quad B_2 \times (-\infty, \infty).$$
 (2.8)

In (2.8)  $\underline{S}$  is the surface traction vector with components  $S_1 = \sigma_{ij} n_j$ , while  $\hat{u}$  and  $\hat{S}$  are prescribed functions.

The mixed boundary-value problem thus consists in finding field histories  $\underline{u},\underline{\varepsilon},\underline{\sigma}$  which, for given  $R,B_{\alpha}$ , known  $\underline{G}$  [or  $\underline{J}$ ], and prescribed  $\underline{F},\underline{\hat{u}},\underline{\hat{S}}$ , satisfy (2.1), (2.2), (2.3) [or (2.4)], (2.6), (2.7), (2.8). We will let  $g = g(R,B_{\alpha},\underline{\hat{u}},\underline{\hat{S}},\underline{F},\underline{G})$  denote the foregoing problem for the case in which the stress-strain relations

are in relaxation integral form - i.e. (2.3) holds. On the other hand, if the stress-strain law is given in the creep integral form (2.4), we will denote this problem by  $\hat{J} = \hat{J}(R, B_{\alpha}, \hat{u}, \hat{S}, F, J)$ .

In order to avoid repeated regularity assumptions concerning the data we define a

Regular problem. We say that  $g = g(R, B_{\alpha}, \hat{u}, \hat{s}, F, \underline{a})$  is a regular problem of relaxation type if:

- (a) R is a bounded region, its boundary B consists of a finite number of non-intersecting closed regular surfaces, and the subsets B are regular surfaces;
- (b) (i)  $\hat{u}$  is a vector-valued function defined on  $B_1 \times (-\infty, \infty)$  which vanishes on  $B_1 \times (-\infty, 0)$  and is uniformly continuous on  $B_1 \times [0,\tau]$  (0 <  $\tau$  <  $\infty$ );
  - (ii)  $\hat{S}$  is a vector-valued function defined on  $B_2 \times (-\infty, \infty)$  which vanishes on  $B_2 \times (-\infty, 0)$  and is uniformly continuous on  $B_2 \times [0,\tau]$  (0 <  $\tau$  <  $\infty$ ) for every regular surface element  $B_2 \subset B_2$ ;
  - (iii) F is a vector-valued function defined on  $R\times(-\infty,\infty)$  which vanishes on  $R\times(-\infty,0)$  and is uniformly continuous on  $R\times[0,\tau]$  (0 <  $\tau$  <  $\infty$ ).
- (c) G is a fourth-order tensor-valued function (of position and time) defined on  $\Re(-\infty,\infty)$  which vanishes on  $\Re(-\infty,0)$ , is continuously differentiable on  $\Re(0,\infty)$ , and has the symmetry properties

$$G_{ijkl} = G_{jikl} = G_{klij} \quad \underline{on} \quad \overline{R} \times (-\infty, \infty).$$
 (2.9)

See Kellogg [14] for the definition of a closed regular surface and the definition of a regular surface element.

We say that  $\mathcal{J} = \mathcal{J}(R, B_{\alpha}, \hat{u}, \hat{S}, F, J)$  is a regular problem of creep type if (a),(b),(c) hold with G replaced by J.

Condition (1) in (b) is equivalent to the requirement that  $\underline{\hat{u}}$  coincide on  $B_1 \times [0,\tau]$  with a function continuous on the closure of  $B_1 \times [0,\tau]$ . The analogous comment applies to (111) in (b). If  $\underline{\hat{S}}$  is the prescribed boundary traction of a problem and  $\underline{\sigma}$  is the stress tensor of the corresponding solution then  $\underline{\hat{S}}_1 = \underline{\sigma}_{1,1} \underline{n}_1$  on  $B_2 \times [0,\infty)$ . This motivates condition (11) in (b) since  $\underline{n}$  has finite jump discontinuities on  $B_2$ , but not on any regular surface element  $B_2 \subset B_2$ .

The first of the symmetry relations appearing in (2.9) is a direct consequence of the symmetry of the stress tensor. The second of (2.9), for the special case of an isotropic solid, follows automatically from the condition that the values of  $\underline{G}$  be isotropic. For the general <u>anisotropic</u> solid this second symmetry relation constitutes an independent assumption.

Our main objective is the characterization of the solution to the foregoing boundary-value problem by means of variational principles. It thus becomes essential to spell out precisely what we mean by a regular solution to the problem. To this end we first give the following definition of an  $\frac{\text{Admissible state. We say that the ordered array } {\$} = [u, \varepsilon, \sigma] \text{ is an admissible state on } \mathbb{R} \times (-\infty, \infty) \text{ if:}$ 

Theoretical support for this assumption has occasionally been based on thermodynamic arguments involving an appeal to Onsager's principle. See Rogers and Pipkin [15] for a discussion of this issue.

(a) <u>u</u> is a vector-valued function defined on  $\mathbb{R} \times (-\infty, \infty)$ , while <u>s</u> and <u>o</u> are symmetric second-order tensor-valued functions <u>defined</u> on  $\mathbb{R} \times (-\infty, \infty)$ ;

(b)  $\underline{u},\underline{\varepsilon},\underline{\sigma}$  vanish on  $\overline{R}\times(-\infty,0)$  and are continuously differentiable on  $\overline{R}\times[0,\infty)$ .

Note that an admissible state is allowed to have finite jump discontinuities at the time origin and need not meet (2.1), (2.2), (2.3), or (2.4). Addition of states and multiplication of a state by a scalar are defined by

$$\mathcal{S} + \tilde{\mathcal{S}} = [\underline{\mathbf{u}} + \tilde{\mathbf{u}}, \underline{\mathbf{e}} + \tilde{\mathbf{e}}, \underline{\mathbf{o}} + \tilde{\mathbf{o}}], \quad \alpha \mathcal{S} = [\underline{\alpha}\underline{\mathbf{u}}, \underline{\alpha}\underline{\mathbf{e}}, \underline{\alpha}\underline{\mathbf{o}}]. \quad (2.10)$$

In view of (2.10) the set of all admissible states on  $\overline{R}\times(-\infty,\infty)$  is a linear space.

We are now ready to introduce the notion of a Regular solution. Let  $g = g(R, B_{\alpha}, \hat{u}, \hat{S}, F, G)$  be a regular problem of relaxation type. Then we say that  $S = [u, \varepsilon, \sigma]$  is a regular solution of g if:

- (a)  $\lambda$  is an admissible state on  $\mathbb{R}\times(-\infty,\infty)$ ;
- (b) <u>u,e,o</u> meet the field equations (2.1),(2.2),(2.3) and satisfy the boundary conditions (2.7),(2.8).

Let  $\int = \int (R, B_{\alpha}, \hat{u}, \hat{S}, F, J)$  be a regular problem of creep type. Then we say that  $\int = [u, \varepsilon, d]$  is a regular solution of  $\int \int f(a)$ , (b) hold with (2.3) replaced by (2.4).

See, for example, Taylor [16] for the definition of a linear space.

Clearly a regular solution is allowed to possess finite jump discontinuities at time zero.

Next we define the

Variation of a functional. Let  $\Omega\{\cdot\}$  be a functional defined on a subset K of a linear space L. Let

$$\tilde{\mathcal{J}} \in L$$
,  $\mathcal{J} + \alpha \tilde{\mathcal{J}} \in K$  for every real number  $\alpha$ , (2.11)

and formally define the notation

$$\delta_{\tilde{g}}\Omega\{\tilde{g}\} = \frac{d}{d\alpha} \Omega\{\tilde{g} + \alpha\tilde{g}\} \Big|_{\alpha=0} . \qquad (2.12)$$

We say that the variation of  $\Omega\{\cdot\}$  is zero at  $\lambda$  and write

$$\delta\Omega\{\} = 0 \quad \underline{\text{over}} \quad K \tag{2.13}$$

whenever  $\delta_{\tilde{g}}\Omega\{l\}$  exists and equals zero for every choice of  $\tilde{g}$  consistent with (2.11).

Unless otherwise specified, the underlying linear space L for the variational principles proved in this paper will be the set of all admissible states on  $\overline{R}\times(-\infty,\infty)$ .

Finally, we will consistently write  $\underline{S}$  and  $\underline{\tilde{S}}$  for the traction vectors with components

$$S_{1} = \sigma_{1j}^{n}, \tilde{S}_{1} = \tilde{\sigma}_{1j}^{n}$$
 (2.14)

respectively.

# 3. Variational principles for problems of relaxation type.

We begin with a generalization of the theorem due to the Hu Hai-chang [8] and Washizu [9] mentioned previously. First variational principle. Let  $\mathcal{G} = \mathcal{G}(R, B_{\alpha}, \hat{u}, \hat{S}, F, G)$  be a regular problem of relaxation type. Let K be the set of all admissible states on  $R \times (-\infty, \infty)$ . Let  $\mathcal{G} = [u, \varepsilon, \sigma] \in K$  and for each fixed  $t \in (-\infty, \infty)$  define the functional  $\Lambda_t \{\cdot\}$  on K through

$$\Lambda_{t}\{\} = \frac{1}{2} \int_{R} [G_{1jk} * de_{1j} * de_{k\ell}](\underline{x}, t) dV_{\underline{x}} - \int_{R} [G_{1j} * de_{1j}](\underline{x}, t) dV_{\underline{x}} 
- \int_{R} [(G_{1j}, j + F_{1}) * du_{1}](\underline{x}, t) dV_{\underline{x}} + \int_{B_{1}} [S_{1} * d\hat{u}_{1}](\underline{x}, t) dA_{\underline{x}} 
+ \int_{B_{2}} [(S_{1} - \hat{S}_{1}) * du_{1}](\underline{x}, t) dA_{\underline{x}}.$$
(3.1)<sup>10</sup>

Then

$$\delta \Lambda_{t} \{ \emptyset \} = 0 \text{ over } K \ (-\infty < t < \infty) \tag{3.2}$$

if and only if  $\[ \]$  is a regular solution of  $\[ \]$ .

Proof: Let  $\[ \] = \[ \[ \] \] \in \mathbb{K}$  from which it follows that  $\[ \] + \alpha \] \in \mathbb{K}$ .

Then by (2.12), (2.9), Theorems 1.2 and 1.6 of [13], and the symmetry of  $\[ \]$ 

We write  $dV_{\underline{x}}$  and  $dA_{\underline{x}}$  for the volume element and element of area, respectively, to indicate that  $\underline{x}$  is the variable of integration.

$$\begin{split} \delta_{\tilde{A}} \Lambda_{t} \{ \hat{b} \} &= \int_{R} \left[ (G_{ijk} \ell^{*de}_{k} \ell^{-d}_{ij})^{*d\tilde{e}}_{ij} \right] (\underline{x}, t) dV_{\underline{x}} + \\ &- \int_{R} \left[ (G_{ij,j}^{+} + F_{i})^{*d\tilde{u}}_{i} \right] (\underline{x}, t) dV_{\underline{x}} + \\ &- \int_{R} \left[ (E_{ij}^{-\frac{1}{2}} (u_{i,j}^{+} + u_{j,i}^{+}))^{*d\tilde{e}}_{ij} \right] (\underline{x}, t) dV_{\underline{x}} + \\ &+ \int_{B_{1}} \left[ (\hat{u}_{i}^{-} - u_{i})^{*d\tilde{s}}_{i} \right] (\underline{x}, t) dA_{\underline{x}} + \\ &+ \int_{B_{2}} \left[ (S_{i}^{-\frac{2}{3}})^{*d\tilde{u}}_{i} \right] (\underline{x}, t) dA_{\underline{x}} \quad (-\infty < t < \infty). \end{split}$$

$$(3.3)$$

First suppose  $\beta$  is a solution of  $\gamma$ . Then by virtue of (2.1), (2.2),(2.3),(2.7),(2.8), equation (3.3) becomes

$$\delta_{\tilde{\ell}} \Lambda_{t} \{ \hat{\ell} \} = 0 \text{ over } K \ (-\infty < t < \infty). \tag{3.4}$$

Equation (3.2) now follows from (3.4) since  $\tilde{\beta} \in K$  was chosen arbitrarily.

Now turn to the "only if" portion of the proof. We must show that  $\hat{S}$  is a regular solution of  $\hat{G}$  whenever  $\hat{S} \in \mathbb{K}$  and (3.4) holds for every  $\hat{S} \in \mathbb{K}$ . In particular choose  $\underline{\tilde{u}}(\underline{x},t) = \underline{u}'(\underline{x})h(t)$ ,  $\underline{\tilde{\varepsilon}}(\underline{x},t) = \underline{\varepsilon}'(\underline{x})h(t)$ ,  $\underline{\tilde{\sigma}}(\underline{x},t) = \underline{\sigma}'(\underline{x})h(t)$ (3.5) for every  $(\underline{x},t) \in \mathbb{R} \times (-\infty,\infty)$ , where h is the Heaviside unit step function, i.e. h(t) = 0 ( $-\infty < t < 0$ ), h(t) = 1 ( $0 \le t < \infty$ ). Therefore (3.4), by virtue of (3.3) and Theorem 1.2 in [13], becomes

$$\int_{R} \left[G_{1jk}\ell^{*}d\varepsilon_{k}\ell^{-}\sigma_{1j}\right](\underline{x},t)\varepsilon_{1j}^{'}(\underline{x})dV_{\underline{x}} - \int_{R} \left[\sigma_{1j},j^{+}F_{1}\right](\underline{x},t)u_{1}^{'}(\underline{x})dV_{\underline{x}} + \int_{R} \left[\varepsilon_{1j}^{-\frac{1}{2}}(u_{1},j^{+}u_{j,1})\right](\underline{x},t)\sigma_{1j}^{'}(\underline{x})dV_{\underline{x}} + \int_{B_{1}} \left[\hat{u}_{1}^{'}-u_{1}\right](\underline{x},t)\sigma_{1j}^{'}(\underline{x})n_{j}(\underline{x})dA_{\underline{x}} + \int_{B_{2}} \left[S_{1}^{-}\hat{S}_{1}\right](\underline{x},t)u_{1}^{'}(\underline{x})dA_{\underline{x}} = 0 \quad (-\infty < t < \infty) \quad (3.6)$$

and (3.6) must hold for every  $\underline{u}',\underline{\varepsilon}',\underline{\sigma}'$  continuously differentiable on  $\overline{R}$  with  $\underline{\varepsilon}'$  and  $\underline{\sigma}'$  symmetric. But this fact, the fundamental lemma of the calculus of variations, and the symmetries of  $\underline{\sigma},\underline{\varepsilon},\underline{G}$  imply that  $\mathring{\mathcal{S}}$  meets (2.1),(2.2),(2.3),(2.8) and that

$$\int_{B_1} \left[ \hat{\mathbf{u}}_1 - \mathbf{u}_1 \right] (\underline{\mathbf{x}}, \mathbf{t}) \sigma_{ij}^{\prime}(\underline{\mathbf{x}}) \mathbf{n}_j(\underline{\mathbf{x}}) dA_{\underline{\mathbf{x}}} = 0 \quad (-\infty < \mathbf{t} < \infty). \quad (3.7)$$

Now assume there exists a regular point  $\underline{x}^{\circ} \in B_{1}$  such that  $\underline{u}(\underline{x}^{\circ},t) \neq \hat{\underline{u}}(\underline{x}^{\circ},t)$  which implies  $u_{k}(\underline{x}^{\circ},t) \neq \hat{u}_{k}(\underline{x}^{\circ},t)$  for some (fixed) k. Choose the coordinate frame such that  $n_{k}(\underline{x}^{\circ}) \neq 0$ , let f be continuously differentiable on  $\overline{R}$ , and let  $\sigma_{1,j}^{i}(\underline{x}) = \delta_{1,k}\delta_{j,k}f(\underline{x})$  (no sum). Then, since (3.7) must hold for every such  $\underline{\sigma}^{i}$ ,  $[u_{k}(\underline{x},t) - \hat{u}_{k}(\underline{x},t)]n_{k}(\underline{x}) = 0$  (no sum) for every  $(\underline{x},t) \in B_{1} \times (-\infty,\infty)$  with  $\underline{x}$  regular, which implies  $u_{k}(\underline{x}^{\circ},t) = \hat{u}_{k}(\underline{x}^{\circ},t)$ . Consequently, we have a contradiction and hence  $\underline{u}(\underline{x},t) = \underline{\hat{u}}(\underline{x},t)$  for every  $(\underline{x},t) \in B_{1} \times (-\infty,\infty)$  with  $\underline{x}$  regular. Thus and by the continuity of  $\underline{u}$  and  $\underline{\hat{u}}$ , (2.7) holds as well and  $\underline{\hat{s}}$  is a solution of  $\underline{\hat{s}}$ . This completes the proof.

By virtue of the divergence theorem,  $\Lambda_{\mbox{\scriptsize t}}$  admits the alternative representation

$$\Lambda_{t} \{ \hat{X} \} = \frac{1}{2} \int_{R} [G_{ijk} \ell^{*d\epsilon}_{ij} \ell^{*d\epsilon}_{k} \ell] (\underline{x}, t) dV_{\underline{x}} - \int_{R} [G_{ij} \ell^{*d}_{ij} \ell^{*d}_{ij}] (\underline{x}, t) dV_{\underline{x}} + \\
- \int_{R} [F_{i} \ell^{*du}_{i}] (\underline{x}, t) dV_{\underline{x}} - \int_{B_{1}} [S_{i} \ell^{*d}_{ij}] dA_{\underline{x}} + \\
- \int_{B_{2}} [\hat{S}_{i} \ell^{*du}_{i}] (\underline{x}, t) dA_{\underline{x}}. \tag{3.8}$$

If, in addition to merely being admissible,  $\mathcal{N} = [\underline{u},\underline{\varepsilon},\underline{\sigma}]$  meets (2.1),(2.3), and (2.7), then  $\Lambda_{\mathbf{t}}\{\mathcal{N}\}$  given by (3.8) reduces to  $\Phi_{\mathbf{t}}\{\mathcal{N}\}$ , where

$$\Phi_{t}\{\} = \frac{1}{2} \int_{R} \left[G_{1jk}\ell^{*d\epsilon}_{1j}^{*d\epsilon}_{k}\ell\right](\underline{x},t)dV_{\underline{x}} - \int_{R} \left[F_{1}^{*du}_{1}\right](\underline{x},t)dV_{\underline{x}} + \int_{B_{2}} \left[\hat{S}_{1}^{*du}_{1}\right](\underline{x},t)dA_{\underline{x}}.$$

$$(3.9)$$

Thus we are led to the following generalization of the principle of stationary potential energy.

Second variational principle. Let  $G = G(R, B_{\alpha}, \hat{\Omega}, \hat{S}, F, G)$  be a regular problem of relaxation type. Let K be the set of all admissible states on  $R\times(-\infty,\infty)$  which meet the strain-displacement relations (2.1), the stress-strain relations (2.3), as well as the displacement boundary conditions (2.7). Let  $S = [\underline{u},\underline{\varepsilon},\underline{\sigma}] \in K$  and for each fixed  $t \in (-\infty,\infty)$  define the functional  $\Phi_t\{\cdot\}$  on K through (3.9). Then

$$\delta\Phi_{\mathbf{t}}\{\}\} = 0 \quad \underline{\text{over}} \quad K \quad (-\infty < t < \infty) \tag{3.10}$$

if and only if & is a regular solution of 9.

<u>Proof</u>: The "if" portion of the proof follows at once from the first variational principle and the discussion preceding (3.9).

To establish the remainder of the theorem assume

$$\delta \Phi_{\mathbf{t}} \{ \} = 0 \quad \text{over} \quad K \quad (-\infty < \mathbf{t} < \infty)$$
 (3.11)

for every  $\tilde{g}$  which meets (2.11). This latter condition is equivalent to the requirement that  $\tilde{g}$  be admissible and meet (2.1),(2.3), with

$$\underline{\tilde{u}} = 0 \text{ on } B_1 \times (-\infty, \infty).$$
 (3.12)

Clearly, (3.3) holds if we replace  $\Lambda_{\mathbf{t}}\{\emptyset\}$  by  $\Phi_{\mathbf{t}}\{\emptyset\}$  and omit the first, third, and fourth terms, since  $\emptyset$  meets (2.1),(2.3), (2.7). Now choose  $\underline{\tilde{u}}(\underline{x},t) = \underline{u}'(\underline{x})h(t)$  for every  $(\underline{x},t)$  in  $\overline{\mathbb{R}}\times(-\infty,\infty)$ , where h is the Heaviside unit step function and  $\underline{u}'$  is twice continuously differentiable on  $\overline{\mathbb{R}}$ , with

$$\underline{\mathbf{u}}^{\mathbf{i}} = 0 \quad \text{on} \quad \mathbf{B}_{\mathbf{i}} \quad . \tag{3.13}$$

Next define continuously differentiable functions  $\frac{\tilde{\epsilon}}{2}, \frac{\tilde{\sigma}}{2}$  on  $\tilde{R}$  through (2.1),(2.3). Thus and by (3.11),

$$-\int_{R} [\sigma_{ij,j}^{\dagger} + F_{i}](\underline{x},t) u_{i}^{\dagger}(\underline{x}) dV_{\underline{x}} + \int_{B_{2}} [S_{1} - \hat{S}_{i}](\underline{x},t) u_{i}^{\dagger}(\underline{x}) dA_{\underline{x}} = 0$$

$$(-\infty < t < \infty) (3.14)$$

for every function  $\underline{u}^{i}$  with the foregoing properties. But this fact, by virtue of the fundamental lemma of the calculus of variations, implies that  $\hat{\lambda}$  meets (2.2),(2.8) and the proof is complete.

Recall our agreement that L is the set of all admissible states on  $\mathbb{R}\times(-\infty,\infty)$ .

# 4. Variational principles for problems of creep type.

Hellinger-Reissner principle in linear elastostatics.

Third variational principle. Let  $\oint = \oint (R, B_{\alpha}, \hat{u}, \hat{S}, F, J)$  be a regular problem of creep type. Let K be the set of all admissible states on  $\overline{R} \times (-\infty, \infty)$  which meet the strain-displacement relations (2.1). Let  $\oint = [\underline{u}, \underline{s}, \underline{\sigma}] \in K$  and for each fixed  $\underline{t} \in (-\infty, \infty)$  define the functional  $\Theta_{\underline{t}} \{\cdot\}$  on K through

The following theorem is a generalization of the

$$\Theta_{\mathbf{t}}\{\} = \int_{\mathbf{R}} \left[\sigma_{\mathbf{1}\mathbf{j}} * d\varepsilon_{\mathbf{1}\mathbf{j}}\right](\underline{\mathbf{x}}, \mathbf{t}) dV_{\underline{\mathbf{x}}} - \frac{1}{2} \int_{\mathbf{R}} \left[J_{\mathbf{1}\mathbf{j}\mathbf{k}\ell} * d\sigma_{\mathbf{1}\mathbf{j}} * d\sigma_{\mathbf{k}\ell}\right](\underline{\mathbf{x}}, \mathbf{t}) dV_{\underline{\mathbf{x}}}$$

$$- \int_{\mathbf{R}} \left[F_{\mathbf{1}} * d\mathbf{u}_{\mathbf{1}}\right](\underline{\mathbf{x}}, \mathbf{t}) dV_{\underline{\mathbf{x}}} - \int_{\mathbf{B}_{\mathbf{1}}} \left[S_{\mathbf{1}} * d(\mathbf{u}_{\mathbf{1}} - \hat{\mathbf{u}}_{\mathbf{1}})\right](\underline{\mathbf{x}}, \mathbf{t}) dA_{\underline{\mathbf{x}}}$$

$$- \int_{\mathbf{B}_{\mathbf{2}}} \left[\hat{S}_{\mathbf{1}} * d\mathbf{u}_{\mathbf{1}}\right](\underline{\mathbf{x}}, \mathbf{t}) dA_{\underline{\mathbf{x}}} . \tag{4.1}$$

Then

$$\delta\Theta_{t}\{\mathcal{J}\} = 0 \quad \underline{\text{over}} \quad K \quad (-\infty < t < \infty) \tag{4.2}$$

if and only if  $\beta$  is a regular solution of  $\beta$ .

<u>Proof</u>: Let  $\tilde{J} = [\tilde{u}, \tilde{\epsilon}, \tilde{d}]$  meet (2.11). Then from the definition of K and since  $\tilde{J} \in K$ , we have that  $\tilde{J} \in K$ . Consequently, because of Theorems 1.2 and 1.6 of [13],

$$\delta_{\widetilde{D}} = \int_{\mathbb{R}} \left[ (\varepsilon_{1j} - J_{1jk\ell} * d\sigma_{k\ell}) * d\widetilde{\sigma}_{1j} \right] (\underline{x}, t) dV_{\underline{x}}$$

$$- \int_{\mathbb{R}} \left[ (\sigma_{1j}, j^{+F_{1}}) * d\widetilde{u}_{1} \right] (\underline{x}, t) dV_{\underline{x}} + \int_{\mathbb{B}_{1}} \left[ \widetilde{S}_{1} * d(\widehat{u}_{1} - u_{1}) \right] (\underline{x}, t) dA_{\underline{x}}$$

$$+ \int_{\mathbb{B}_{2}} \left[ (S_{1} - \widehat{S}_{1}) * d\widetilde{u}_{1} \right] (\underline{x}, t) dA_{\underline{x}} \quad (-\infty < t < \infty). \quad (4.3)$$

<sup>12</sup> See the previous footnote.

The conclusion now follows from (4.3) by an argument which is strictly analogous to that which led from (3.3) to the final conclusion in the proof of the first variational principle.

We turn next to a generalization of the principle of stationary complementary energy in elastostatics. With a view toward an economical statement of this generalized principle we introduce the subsequent notions.

Convexity of R with respect to B<sub>1</sub>. We say that R is convex with respect to B<sub>1</sub> if the straight line

$$\underline{x}(\tau) = \hat{\underline{x}} + (\tilde{\underline{x}} - \hat{\underline{x}})\tau \quad (-\infty < \tau < \infty) \quad (4.4)$$

intersects B only at  $\underline{\hat{x}}$  and  $\underline{\tilde{x}}$  whenever  $\underline{\hat{x}}$ ,  $\underline{\tilde{x}} \in B_1$ .

Notice that if  $B = B_2$  then R is automatically convex with respect to  $B_1$ .

Admissible stress field. We say that  $\sigma$  is an admissible stress field on  $\overline{R}\times(-\infty,\infty)$  if  $\sigma$  is a symmetric second-order tensor-valued function defined on  $\overline{R}\times(-\infty,\infty)$ , which vanishes on  $\overline{R}\times(-\infty,0)$  and is continuously differentiable on  $\overline{R}\times[0,\infty)$ .

Finally, we stipulate that the underlying linear space L for the following theorem is the set of all admissible stress fields on  $\overline{R}x(-\infty,\infty)$ .

Fourth variational principle. Let  $\int = \int (R,B_{\alpha},\hat{u},\hat{S},F,J)$  be a regular problem of creep type. Let K be the set of all admissible stress-fields on  $R\times(-\infty,\infty)$  which meet the stress equations of equilibrium (2.2) and the traction boundary conditions (2.8). Let  $\sigma\in K$  and for each fixed  $t\in (-\infty,\infty)$  define the functional  $\Psi_{t}\{\cdot\}$  on K through

$$\Psi_{t}\{\underline{\sigma}\} = \frac{1}{2} \int_{R} [J_{1jk\ell} * d\sigma_{1j} * d\sigma_{k\ell}](\underline{x}, t) dV_{\underline{x}} - \int_{B_{1}} [S_{1} * d\hat{u}_{1}](\underline{x}, t) dA_{\underline{x}}. \quad (4.5)$$

Then

$$\delta\Psi_{t}\{\underline{\sigma}\} = 0 \text{ over } K \ (-\infty < t < \infty) \tag{4.6}$$

if there exist functions  $u, \varepsilon$  such that  $[u, \varepsilon, \sigma]$  is a regular solution of  $\hat{y}$ .

#### Conversely, suppose

- (a) R is convex with respect to B1;
- (b) R is simply-connected;
- (c)  $\underline{J}$  and  $\underline{d}$  are twice continuously differentiable on  $\mathbb{R}\times[0,\infty)$ ;
- (d)  $\underline{\hat{\mathbf{u}}}(\underline{\mathbf{x}}, \cdot)$ , for each  $\underline{\mathbf{x}} \in \mathbb{B}_1$ , is continuously differentiable on  $[0, \infty)$ ;
- (e) (4.6) holds.

Then there exist functions  $u, \varepsilon$  such that  $[u, \varepsilon, \sigma]$  is a regular solution of  $\mathcal{L}$ .

<u>Proof</u>: Let  $\underline{\tilde{a}} \in L$ ,  $\underline{a} + \alpha \underline{\tilde{a}} \in K$  for every real  $\alpha$ . Then

$$\tilde{\sigma}_{ij,j} = 0 \text{ on } \mathbb{R} \times (-\infty, \infty),$$

$$\tilde{S}_{i} \equiv \tilde{\sigma}_{ij} n_{j} = 0 \text{ on } \mathbb{B}_{2} \times (-\infty, \infty).$$

$$(4.7)$$

Further, since  $J_{ijkl} = J_{klij}$ , it follows that

$$\delta_{\underline{\tilde{g}}}^{\Psi}_{t}\{\underline{\sigma}\} = \int_{\mathbb{R}} [J_{1jk}\ell^{*d\sigma}_{k}\ell^{*d\tilde{\sigma}}_{ij}](\underline{x},t)dV_{\underline{x}} - \int_{\mathbb{R}_{1}} [\tilde{S}_{1}^{*d\hat{u}_{1}}](\underline{x},t)dA_{\underline{x}}$$

$$(-\infty < t < \infty).(4.8)$$

Now suppose there exist functions  $\underline{u}$  and  $\underline{\varepsilon}$  such that  $[\underline{u},\underline{\varepsilon},\underline{\sigma}]$  is a solution of  $\mathcal{Y}$ . Then, by virtue of (4.7) and the divergence theorem, equation (4.8) implies

$$\delta_{\underline{\sigma}^{\Psi} \mathbf{t}} \{\underline{d}\} = 0 \quad (-\infty < \mathbf{t} < \infty). \tag{4.9}$$

Thus, and since  $\frac{\tilde{c}}{2}$  was chosen arbitrarily, (4.6) holds.

We turn next to the proof of the converse assertion. To this end we state and prove the following trivial modification of a theorem due to Dorn and Schild [4].

Let  $\hat{u}$  be a vector-valued function which is uniformly continuous on  $B_1$  and let  $\underline{\varepsilon}$  be a symmetric second-order tensor-valued function which is twice continuously differentiable on  $\overline{R}$ . Further suppose

$$\int_{R} \sigma_{1j}(\underline{x}) \varepsilon_{1j}(\underline{x}) dA_{\underline{x}} = \int_{B_{1}} \sigma_{1j}(\underline{x}) \hat{u}_{1}(\underline{x}) n_{j}(\underline{x}) dA_{\underline{x}}$$
 (4.10)

for every symmetric second-order tensor-valued function of which is continuously differentiable arbitrarily often on R and meets

$$\begin{aligned}
 \sigma_{ij,j} &= 0 & \underline{\text{on }} R, \\
 \sigma_{ij} n_j &= 0 & \underline{\text{on }} B_2.
 \end{aligned}$$
(4.11)

Then there exists a vector-valued function u which is continuously differentiable on R and satisfies

$$2\varepsilon_{i,j} = u_{i,j} + u_{j,i} \quad \underline{on} \quad R$$

$$u_{i} = \hat{u}_{i} \quad \underline{on} \quad B_{i}$$

$$(4.12)$$

<u>Proof</u>: Here we follow the argument of Dorn and Schild. Let  $\underline{g}$  be a <u>symmetric</u> second-order tensor-valued function which is continuously differentiable arbitrarily often on  $\overline{R}$  and which vanishes identically outside a closed subregion of R. Let  $\gamma_{ijk}$ 

denote the usual alternating symbol and define o through

$$\sigma_{ij} = \gamma_{ipq}\gamma_{jrs}g_{pr,qs}$$
 on R, (4.13)

i.e. use  $\underline{g}$  as a Gwyther-Finzi stress function. This choice of  $\underline{\sigma}$  meets (4.11), has the requisite degree of smoothness, and vanishes on B. Therefore (4.10) implies

$$\int_{\mathbb{R}} \varepsilon_{ij} \gamma_{ipq} \gamma_{jrs} g_{pr,qs} dV = 0 . \qquad (4.14)$$

Now integrate (4.14) twice by parts and use the fact that  $\underline{g}$  and all of its partial derivatives vanish on B to deduce that

$$\int_{R} (\gamma_{1pq} \gamma_{jrs} \epsilon_{1j,qs}) g_{pr} dV = 0. \qquad (4.15)$$

Since (4.15) must hold for every such function g

$$\gamma_{piq}\gamma_{r,js}\epsilon_{i,j,qs} = 0 \text{ on } R$$
. (4.16)

Hence  $\underline{\varepsilon}$  is a compatible strain field and from the simple-connectivity of R we conclude that there exists a vector-valued function  $\underline{u}^{'}$  which is continuously differentiable on  $\overline{R}$  and meets

$$2\varepsilon_{ij} = u_{i,j}^{i} + u_{j,i}^{i}$$
 on R. (4.17)

Moreover, such a  $\underline{u}^{i}$  is given by the line integrals  $^{14}$ 

$$u_1^{i}(\underline{x}) = \int_{\underline{x}^{0}}^{\underline{x}} U_{1j}(\underline{\xi},\underline{x}) d\xi_j \quad \text{for every } \underline{x} \in \overline{R} ,$$
 (4.18)

where  $\underline{x}^{0} \in \mathbb{R}$  and for every  $(\underline{\xi},\underline{x}) \in \overline{\mathbb{R}} \times \overline{\mathbb{R}}$ 

<sup>13</sup> See, for instance, Truesdell and Toupin [17] (Article 227).

<sup>14</sup> See, for example, Sokolnikoff [1] (Article 10).

$$U_{\underline{i}\underline{j}}(\underline{\xi},\underline{x}) = \varepsilon_{\underline{i}\underline{j}}(\underline{\xi}) + (x_{\underline{k}} - \xi_{\underline{k}}) [\varepsilon_{\underline{i}\underline{j},\underline{k}}(\underline{\xi}) - \varepsilon_{\underline{k}\underline{j},\underline{i}}(\underline{\xi})]. \quad (4.19)$$

Now let

$$v_{i} = \hat{u}_{i} - u_{i}^{\dagger}$$
 on  $B_{i}$  (4.20)

and use (4.10),(4.11),(4.12), together with the divergence theorem, to establish that

$$\int_{B_1} \sigma_{1j} n_j v_1 dA = 0 . \qquad (4.21)$$

Our next step will be to show that  $\underline{v}$  is a rigid displacement field. To this end let  $\hat{\underline{x}}$  and  $\tilde{\underline{x}}$  be arbitrary interior points of  $B_1$  and choose the coordinate system such that

$$\frac{\hat{x}}{\hat{x}} = (0,0,0), \quad \frac{\tilde{x}}{\hat{x}} = (0,0,\tilde{x}_3). \quad (4.22)$$

Let  $T_{\epsilon}$  be a disc in the  $x_1, x_2$ -plane with radius  $\epsilon$  and center at  $x_1 = x_2 = 0$  and let

$$\sigma_{11}(x_1, x_2, x_3) = \delta_{13}\delta_{13}f_{\epsilon}(x_1, x_2),$$
 (4.23)

where  $f_{\epsilon}$  is defined on the entire  $x_1, x_2$ -plane and has the following properties:

(a) 
$$f_{\epsilon}$$
 is differentiable arbitrarily often;  
(b)  $f_{\epsilon} \geq 0$ ;  
(c)  $f_{\epsilon} = 0$  outside  $D_{\epsilon}$ ;  
(d)  $\int_{C} f_{\epsilon} dA = 1$ .

Clearly such a <u>d</u> meets the first of (4.11). Now let  $C_{\epsilon}$  be the solid circular cylinder whose axis coincides with the  $x_3$ -axis and whose cross-section is  $D_{\epsilon}$ . By the assumed convexity of R

with respect to B1

$$(C_{\varepsilon} \cap B) \subset B_1$$
, (4.25)

for sufficiently small  $\varepsilon$  (say  $\varepsilon < \varepsilon_0$ ). Thus and by (4.23), (4.24), the second of (4.11) holds for  $\varepsilon < \varepsilon_0$ . Further for  $\varepsilon < \varepsilon_1 \le \varepsilon_0$  there exist disjoint subregions  $\hat{\mathcal{B}}_{\varepsilon}$ ,  $\tilde{\mathcal{B}}_{\varepsilon}$  of  $B_1$  such that

$$\underline{\hat{\mathbf{x}}} \in \hat{\mathcal{B}}_{\varepsilon} , \underline{\tilde{\mathbf{x}}} \in \tilde{\mathcal{B}}_{\varepsilon} , \mathbf{c}_{\varepsilon} \cap \mathbf{B}_{1} = \hat{\mathcal{B}}_{\varepsilon} \cup \tilde{\mathcal{B}}_{\varepsilon}. \tag{4.26}$$

Consequently, by virtue of (4.23), (4.24c), equation (4.21) reduces to

$$\int_{\mathcal{B}_{\varepsilon}} f_{\varepsilon} v_{3} n_{3} dA + \int_{\mathcal{B}_{\varepsilon}} f_{\varepsilon} v_{3} n_{3} dA = 0 \quad (\varepsilon < \varepsilon_{1}). \quad (4.27)$$
Next let  $\underline{m} = (0,0,1)$  be the unit normal vector of  $D_{\varepsilon}$  and conclude

Next let  $\underline{m} = (0,0,1)$  be the unit normal vector of  $D_{\varepsilon}$  and conclude from (4.23), (4.24d) that

$$\int_{\mathcal{B}_{\varepsilon}} f_{\varepsilon} n_{3} dA = \int_{\mathcal{B}_{\varepsilon}} \sigma_{ij} n_{j} dA = \int_{D_{\varepsilon}} \sigma_{ij} m_{j} dA = \int_{D_{\varepsilon}} f_{\varepsilon} dA = 1,$$

$$\int_{\mathcal{B}_{\varepsilon}} f_{\varepsilon} n_{3} dA = \int_{\mathcal{B}_{\varepsilon}} \sigma_{ij} n_{j} dA = -\int_{D_{\varepsilon}} \sigma_{ij} m_{j} dA = -\int_{D_{\varepsilon}} f_{\varepsilon} dA = -1,$$

$$(4.28)$$

provided  $\varepsilon < \varepsilon_1$ . Now let  $\varepsilon \rightarrow 0$  in (4.27) and use (4.24b), (4.28) to infer that

$$v_3(\underline{\hat{x}}) - v_3(\underline{\tilde{x}}) = 0. \tag{4.29}$$

But (4.29), because of (4.22) and since  $\hat{x}$ ,  $\hat{x}$  were chosen arbitrarily, implies

$$[\underline{\mathbf{v}}(\hat{\mathbf{x}}) - \underline{\mathbf{v}}(\tilde{\mathbf{x}})] \cdot [\hat{\mathbf{x}} - \tilde{\mathbf{x}}] = 0 \tag{4.30}$$

for every  $\hat{x}$ ,  $\tilde{x} \in B_1$ . Hence  $\underline{v}$  on  $B_1$  must belong to the moment field of a bound vector system and thus admits the representation  $a_1 = a_2 + a_3 = a_4 + a_5 = a_$ 

See, for example, Nielsen [18] (Chapter 3).

$$v_1(\underline{x}) = a_1 + \omega_{1j}x_j \quad (a_1, \omega_{1j} = -\omega_{j1}....constant)$$
 (4.31)

for  $\underline{x} \in B_1$ . Now define  $\underline{u}$  on  $\overline{R}$  through

$$u_{\underline{1}}(\underline{x}) = u_{\underline{1}}^{i}(\underline{x}) + a_{\underline{1}} + \omega_{\underline{1}j}x_{\underline{j}} \text{ if } \underline{x} \in \overline{\mathbb{R}}$$
 (4.32)

and conclude from (4.17), (4.20), (4.31) that  $\underline{u}$  meets (4.12). This completes the proof of the lemma.

We turn now to the remainder of the proof of the fourth variational principle. To this end suppose hypotheses (a) through (e) hold. Clearly, (4.8) is satisfied by every admissible stress field  $\tilde{\underline{\sigma}}$  which meets (4.7). In particular let  $\tilde{\sigma}_{ij}(\underline{x},t) = \sigma_{ij}^i(\underline{x})h(t)$  for every  $(\underline{x},t) \in \overline{R} \times (-\infty,\infty)$ . (4.33) Next define  $\underline{\varepsilon}$  on  $\overline{R} \times (-\infty,\infty)$  through

$$\varepsilon_{ij} = J_{ijkl} * d\sigma_{kl}$$
 (4.34)

and observe that hypothesis (c) and Theorem 1.6 of [13] imply that  $\underline{\varepsilon}$  vanishes on  $\overline{\mathbb{R}}\times(-\infty,0)$  and is twice continuously differentiable on  $\overline{\mathbb{R}}\times[0,\infty)$ . Further, infer from (4.6), (4.8), (4.33), (4.34) that

$$\int_{R} \sigma_{1,j}^{i}(\underline{x}) \varepsilon_{1,j}(\underline{x},t) dV_{\underline{x}} = \int_{B_{1}} \sigma_{1,j}^{i}(\underline{x}) \hat{u}_{1}(\underline{x},t) n_{j}(\underline{x}) dA_{\underline{x}} \quad (-\infty < t < \infty) (4.35)$$

for every  $\underline{\sigma}'$  which is twice continuously differentiable on  $\overline{R}$  and meets

$$\begin{cases}
\sigma_{ij,j}^{i} = 0 & \text{on } R, \\
\sigma_{ij}^{i} n_{j} = 0 & \text{on } B_{2}.
\end{cases}$$
(4.36)

Equations (4.35), (4.36), together with the preceding lemma imply the existence of a displacement field  $\underline{u}$  which satisfies (2.1), (2.7). Moreover, it is clear from the smoothness of  $\underline{\varepsilon}$ , hypothesis (d), and the proof of the lemma that  $\underline{u}$  vanishes on  $\overline{\mathbb{R}}\times(-\infty,0)$ , and is continuously differentiable on  $\overline{\mathbb{R}}\times[0,\infty)$ . Thus we have shown that  $[\underline{u},\underline{\varepsilon},\underline{\sigma}]$  is a regular solution of  $\mathcal{L}$  and the proof is complete.

# References

- [1] I.S. Sokolnikoff, Mathematical theory of elasticity, Second Ed., McGraw-Hill, New York, 1956.
- [2] R.V. Southwell, <u>Castigliano's principle of minimum strainenergy</u>, Proc. R. Soc. London, Ser. A, 154(1936), 4.
- [3] H.L. Langhaar, The principle of complementary energy in nonlinear elasticity theory. J. Franklin Inst., 256 (1953), 16, 255.
- [4] W.S. Dorn and A. Schild, A converse of the virtual work theorem for deformable solids, Quart. Appl. Math., 14 (1956), 2, 209.
- [5] E. Hellinger, <u>Die Allgemeinen Ansätze der Mechanik der Kontinua</u>, in <u>Encyklopädie der Mathematischen Wissenschaften</u>, 4. Part 4 (1914), 5, 654.
- [6] E. Reissner, On a variational theorem in elasticity, J. Math. Phys., 29(1950), 2, 90.
- [7] E. Reissner, On variational principles in elasticity,
  Proceedings of symposia in applied mathematics, Vol. 8,
  Calculus of variations and its applications, McGrawHill, New York, 1958.
- [8] Hu Hai-chang, On some variational principles in the theory of elasticity and the theory of plasticity, Sc. Sinica, 4(1955), 1, 33.
- [9] K. Washizu, On the variational principles of elasticity and plasticity, Rept. 25-18, Cont. N5ori-07833, Massachusetts Institute of Technology, March 1955.
- [10] M.A. Biot, <u>Variational and Lagrangian methods in visco-elasticity</u>, in <u>Deformation and flow of solids</u>, <u>Springer</u>, <u>Berlin</u>, 1955.
- [11] A.M. Freudenthal and H. Geiringer, The mathematical theories of the inelastic continuum, in Encyclopedia of physics, Vol. 6, Springer, Berlin, 1958.
- [12] E.T. Onat, On a variational principle in linear viscoelasticity, J. Mec., 1(1962), 2, 135.
- [13] M.E. Gurtin and E. Sternberg, On the linear theory of viscoelasticity, Rept. No. 6, Cont. Nonr 562(30), Brown University, June 1962, To appear in the Arch. Rat. Mech. Anal.

- [14] O.D. Kellogg, Foundations of potential theory, Springer, Berlin, 1929.
- [15] T.G. Rogers and A.C. Pipkin, <u>Asymmetric relaxation and compliance matrices in linear viscoelasticity</u>, Rept. No. 83, Contract Nonr 562(10), Brown University, July 1962, to appear in Z. angew. Math. Mech.
- [16] A.E. Taylor, <u>Introduction to functional analysis</u>, John Wiley, New York, 1961.
- [17] C. Truesdell and R. Toupin, The classical field theories, in Encyclopedia of physics, Vol. 3, Springer, Berlin, 1960.
- [18] J. Nielsen, Elementare Mechanik, Springer, Berlin, 1935.